

LORENZINI WATERFRONT HOUSE - HIGH ROOF LATERAL DESIGN  
 HOUSE IS 'U' SHAPED W/ CENTER ROOF SET ABOVE SIDE ROOFS &  
 OPPOSING PITCHES

ROOF SHEAR DISTRIBUTION

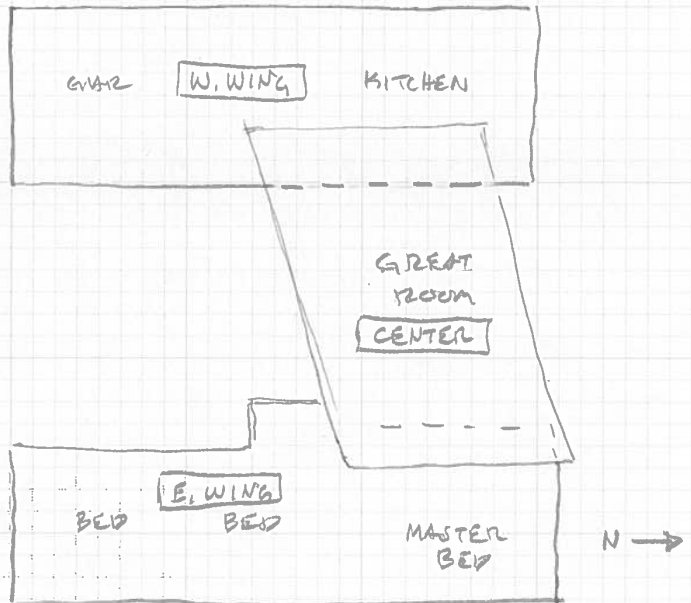
ROOF WT BY WING

W. WING =  $24.9k = 24.6\%$   
 CENTER WING =  $39.4k = 39.0\%$   
 E. WING =  $36.8k = 36.4\%$

Resulting DIAPHRAGM LOADS

$V_R = 28.12k$   
 $\therefore$  WEST =  $6.92k$   
 CENTER =  $10.97k$   
 EAST =  $10.24k$

(BASED ON  $R = 6.5$ )



CENTER 'HIGH' ROOF LATERAL LOADS ARE RESISTED BY  
 SHEAR WALLS AT INTERSECTIONS W/ WING ROOFS AND AT  
 FULL PLATE ELEMENTS C.F.P.  
 STEEL FRAME & TRUSSES AT CENTER WING ARE NOT DESIGNED  
 TO RESIST LATERAL LOADS BY THEMSELVES

PER ASCE 7 SEC 12.3.3.4, DUE TO RE-ENTRANT CORNER CONDITION  
 DESIGN FORCES IN COLLECTORS & THEIR CONNECTIONS ARE  
 INCREASED BY 25% (TYPE 2 HORIZONTAL IRREGULARITY)



I.L. GROSS  
 STRUCTURAL  
 ENGINEERS

REVISED LATERAL DESIGN

SHEET TITLE

SCALE

DATE

PROJECT

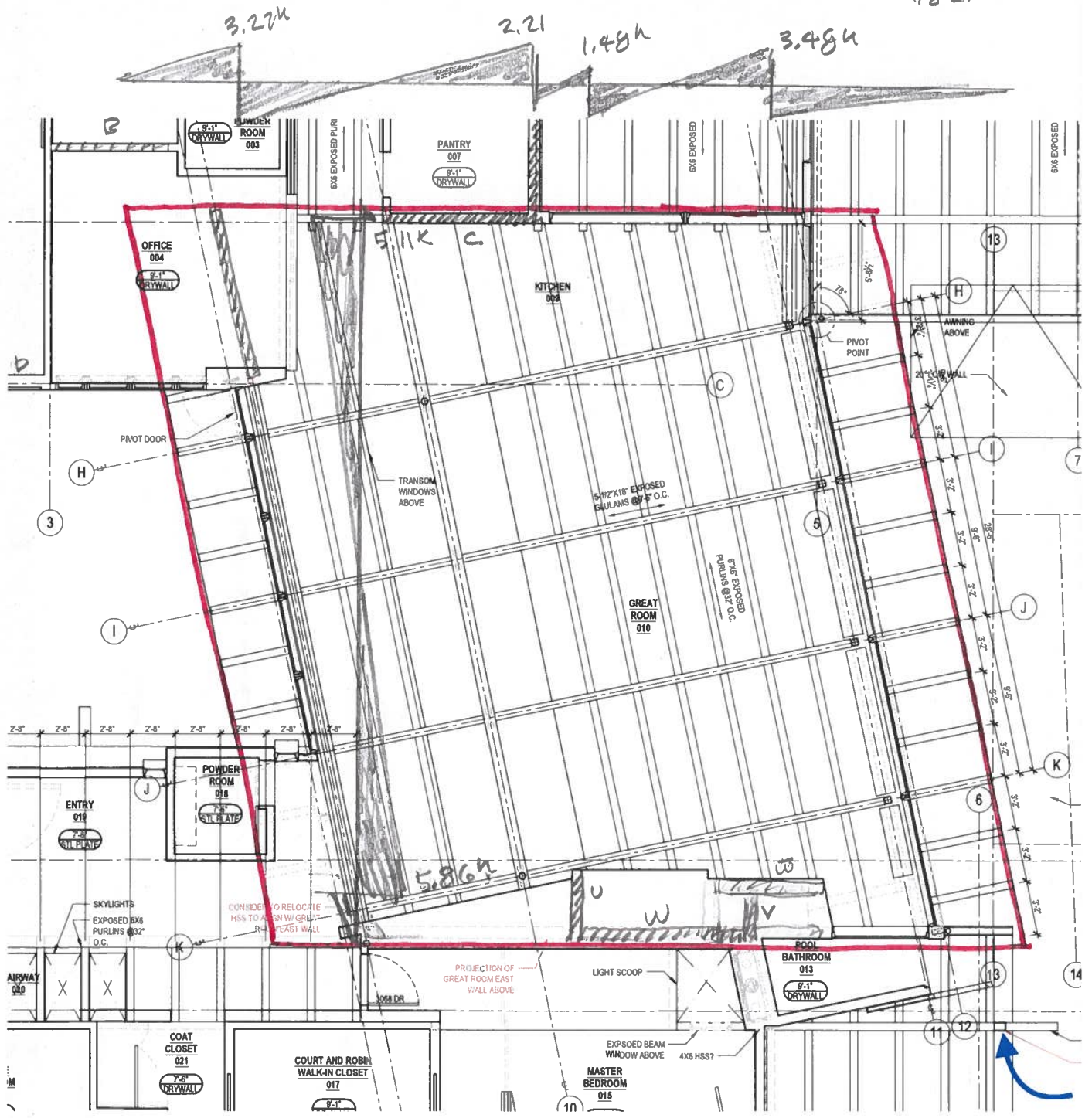
DESIGNED BY

CLIENT

CHECKED

SHEET

DN CENTER HIGH ROOF  
DIAPHRAGM - V2 10.97k  
1/8"=1'



3.27k

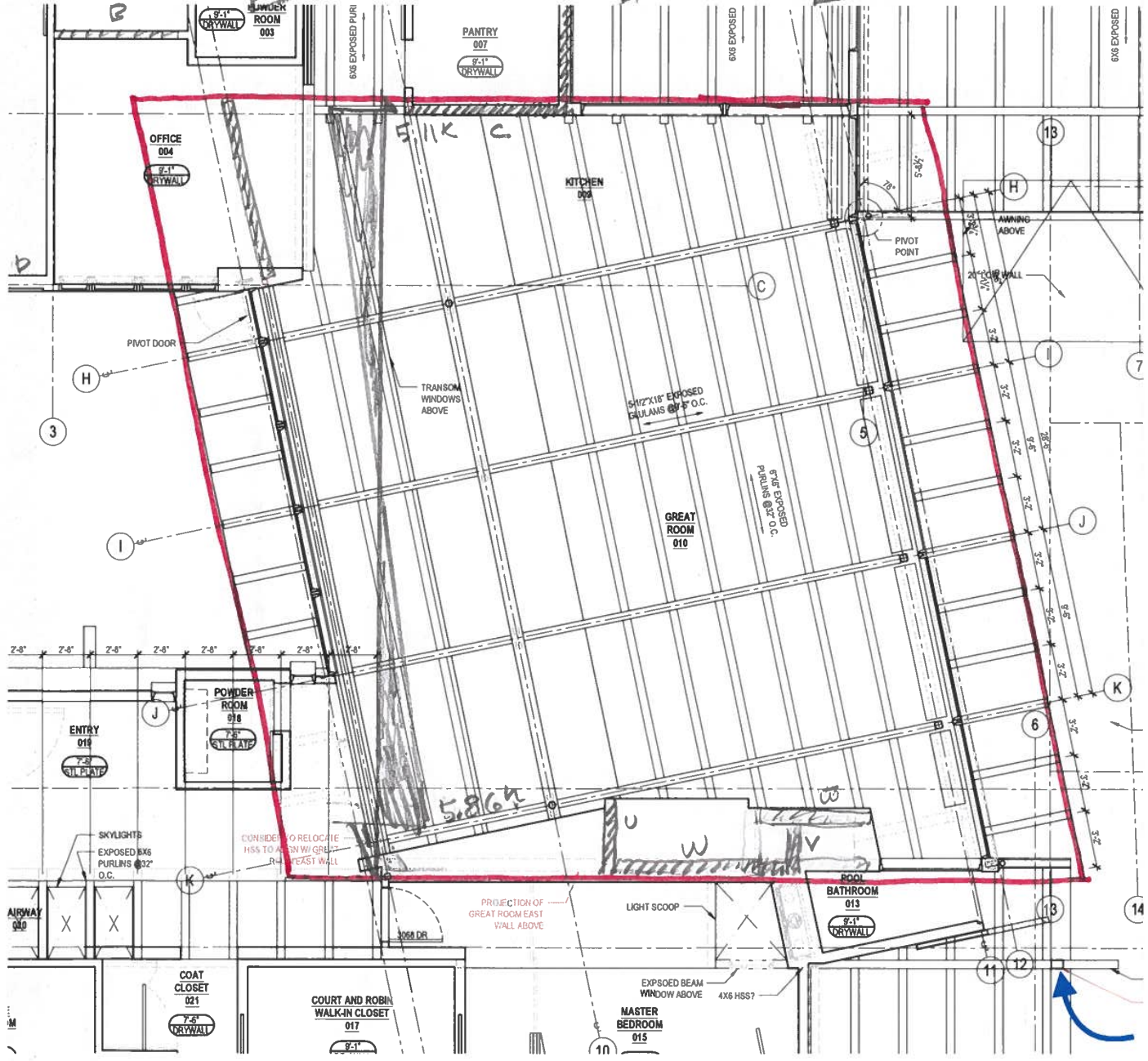
2.21

1.48k

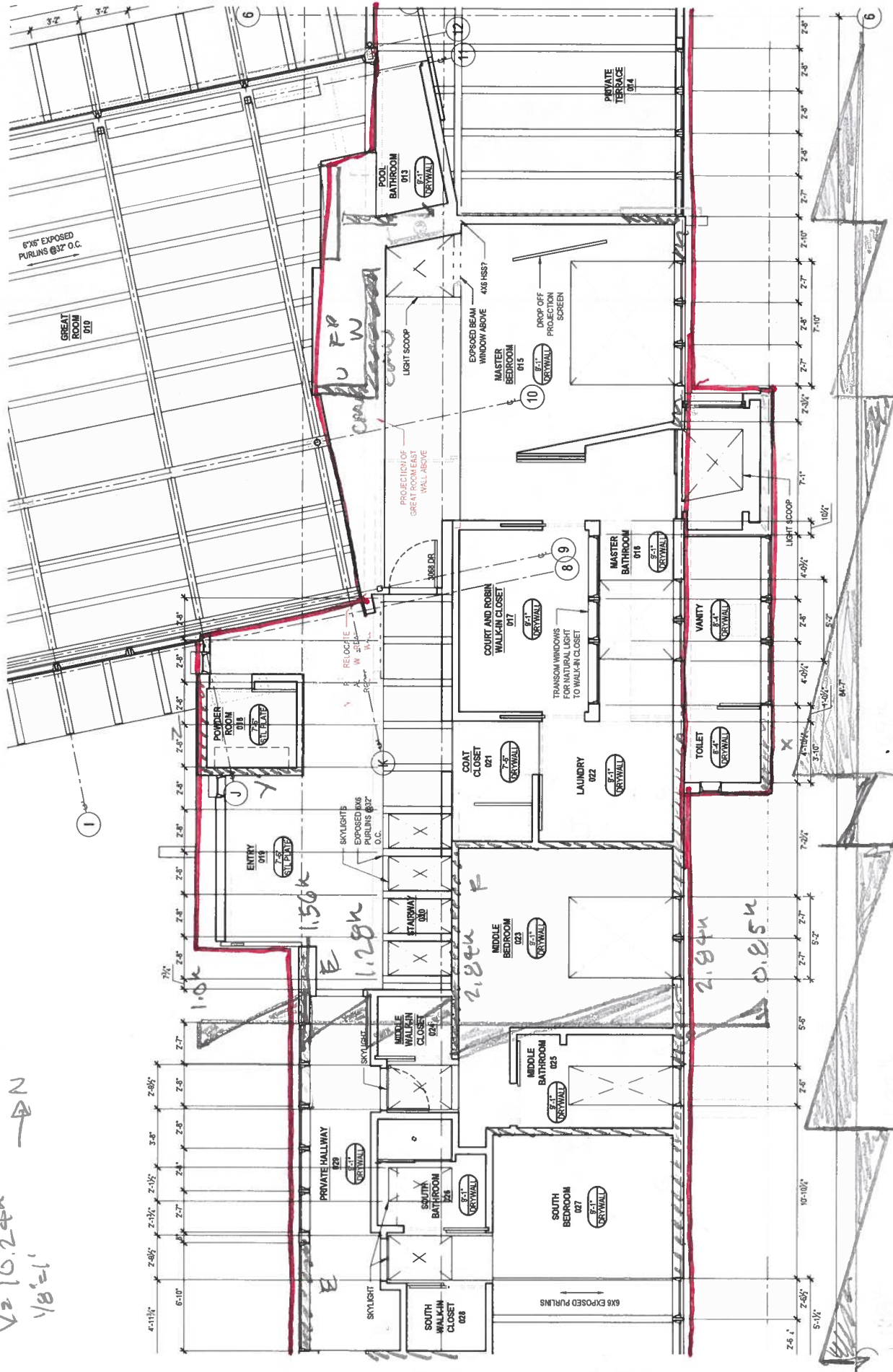
3.48k

5.11k C

5.86k



EAST WING HIGH RISE  
 V=16.24k  
 1/8"=1'

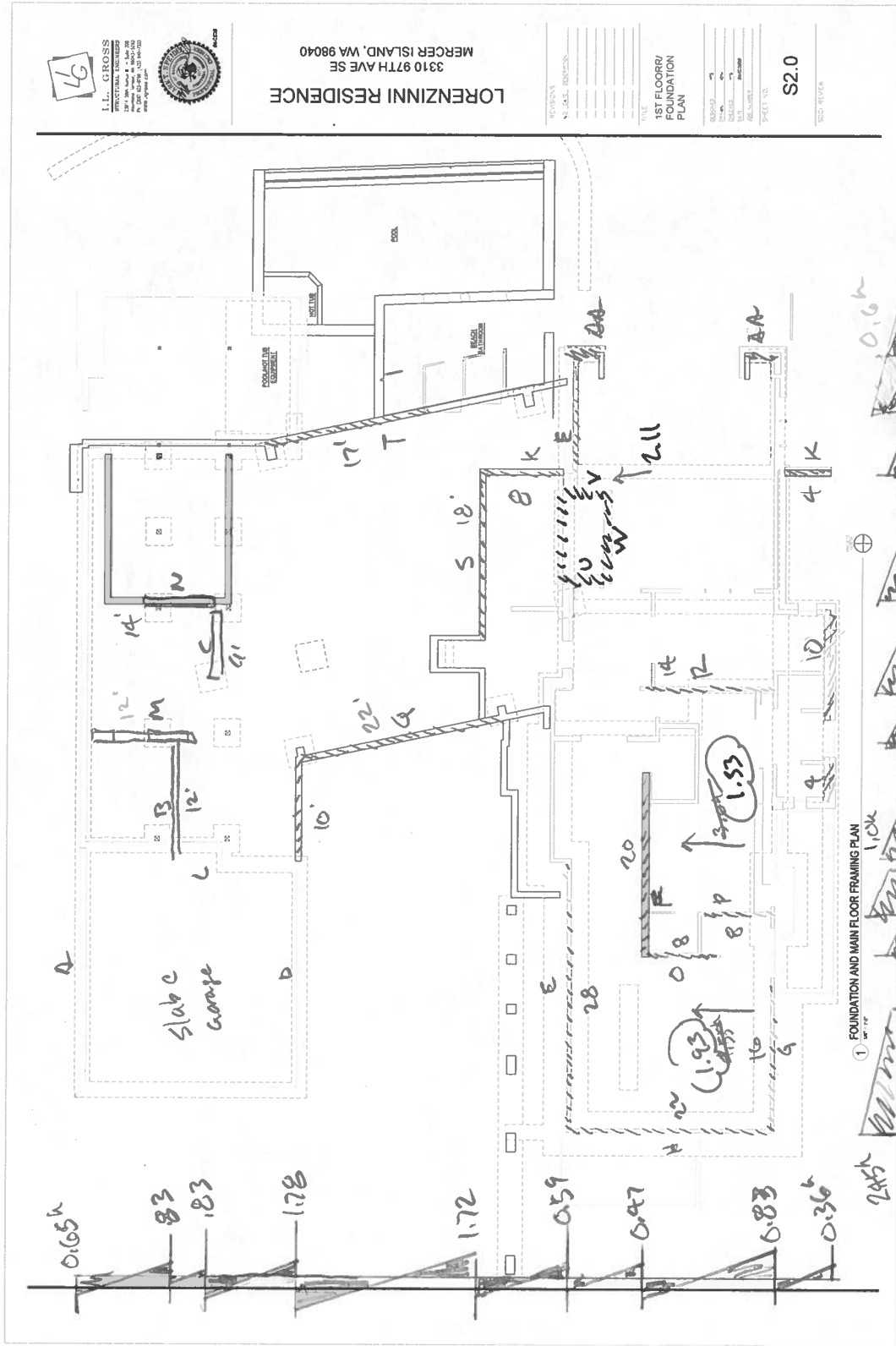


1 MAIN LEVEL REFLECTED CEILING PLAN



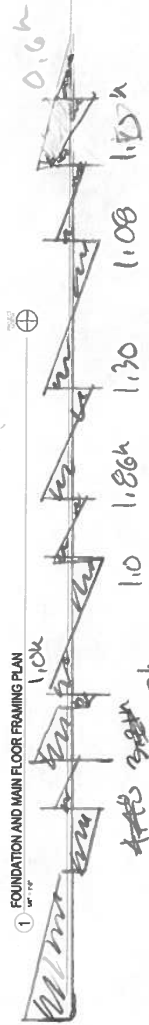
$V_{max} = 9.724$  (SEISMIC)

(Revised Slab)



① FOUNDATION AND MAIN FLOOR FRAMING PLAN

2.73  $\approx$  2.04h  
~~1.10~~ 1.10  
 1.86h 1.30 1.08 1.15h



# Lorenzini House

## Shear wall analysis

LRFD Wood Shear Wall Design

loads  
 wall weight= 12 psf      roof weight= 14.5 psf  
 conc wall= 75 psf      floor weight= 16.5 psf

SW SCHEDULE CAP (plf)

W6	416
W4	600
W3	780
W2	1020
2W4	1215
2W3	1560
TOO HIGH	1600

Holdowns Capacity Straps Capacity

ABs ok	0.6 k	LSTA24	1.2 k
HDU2	3.5 k	LSTA36	2 k
HDU4	5.9 k	MSTC40	3.9 k
HDU5	7.3 k	MSTC66	7.5 k
HDU8	10.2 k	MST72	8.7 k
HDU11	14.4 k	HDU8	10.2 k

Capacities are adjusted fro LRFD values

SW - A N/S Direction

Roof- Upper Floor

H=	12.0	Mot=	59.3 k-ft
L=	46.0	C=	1.3 k
Vapp=	4.9	Mres=	206.2 k-ft
WW=	6.0	T=	0.0 k
TA=	5.0	AR=	1.2
Weight=	3.0	Co=	1.0

Shear VLF= 107.4      **W6 LSTA24**

SW - B N/S Direction

Roof- Upper Floor

H=	10.0	Mot=	25.2 k-ft
L=	8.0	C=	3.2 k
Vapp=	2.5	Mres=	7.6 k-ft
WW=	0.9	T=	2.2 k
TA=	10.0	AR=	1.1
Weight=	1.0	Co=	1.0

Shear VLF= 315.0      **W6 MSTC40**

Upper- Main Floor

H=	6.0	Mot=	92.8 k-ft
L=	46.0	C=	2.0 k
Vapp=	0.7	Mres=	306.1 k-ft
WW=	8.9	T=	0.0 k
TA=	2.0	AR=	1.2
Weight=	4.4	Co=	1.0

Shear VLF= 121.5      **W6 ABs ok**

Foundation Wall at CrawlSpace

Upper- Main Floor

H=	6.0	Mot=	45.3 k-ft
L=	12.0	C=	3.8 k
Vapp=	0.8	Mres=	18.3 k-ft
WW=	1.6	T=	2.3 k
TA=	2.0	AR=	1.2
Weight=	1.4	Co=	1.0

Shear VLF= 279.2      **W6 HDU2**

SW - C E/W Direction

High Roof - low Roof

H=	3.5	Mot=	17.89 k-ft
L=	8.0	C=	2.236 k
Vapp=	5.1	Mres=	3.3 k-ft
WW=	0.3	T=	1.8 k
TA=	5.0	AR=	1.2
Weight=	0.5	Co=	1.0
Shear VLF=		638.8	
<b>W3 LSTA36</b>			

SW - D N/S Direction

Low Roof - Foundation

H=	9.0	Mot=	33.0 k-ft
L=	24.0	C=	1.4 k
Vapp=	3.7	Mres=	50.5 k-ft
WW=	2.3	T=	0.0 k
TA=	6.0	AR=	1.2
Weight=	1.9	Co=	1.0
Shear VLF=		152.9	
<b>W6 ABs ok</b>			

Upper- Main Floor

H=	10.0	Mot=	58.6 k-ft
L=	8.0	C=	7.325 k
Vapp=	0.4	Mres=	10.6 k-ft
WW=	1.2	T=	6.0 k
TA=	8.0	AR=	1.1
Weight=	1.5	Co=	1.0
Shear VLF=		688.8	
<b>W3 HDU5</b>			


Main Floor - Foundation

H=	5.0	Mot=	110.5 k-ft
L=	9.0	C=	12.28 k
Vapp=	0.8	Mres=	15.3 k-ft
WW=	1.7	T=	10.6 k
TA=	2.0	AR=	1.2
Weight=	1.7	Co=	1.0
Shear VLF=		701.1	
<b>W3 HDU11</b>			

SW - E N/S Direction

Roof- Upper Floor			
H=	10.0	Mot=	20.2 k-ft
L=	10.0	C=	2.0 k
Vapp=	2.0	Mres=	8.0 k-ft
WW=	1.1	T=	1.2 k
TA=	4.0	AR=	1.1
Weight=	0.5	Co=	1.0
Shear VLF=		202.0	<b>W6 LSTA36</b>

SW - F N/S Direction

Roof- Upper Floor			
H=	10.0	Mot=	37.0 k-ft
L=	14.0	C=	2.6 k
Vapp=	3.7	Mres=	20.8 k-ft
WW=	1.5	T=	1.2 k
TA=	8.0	AR=	1.2
Weight=	1.5	Co=	1.0
Shear VLF=		264.3	<b>W6 LSTA24</b>

Upper- Main Floor			
H=	9.0	Mot=	43.7 k-ft
L=	40.0	C=	1.1 k
Vapp=	0.6	Mres=	157.3 k-ft
WW=	5.0	T=	0.0 k
TA=	4.0	AR=	1.2
Weight=	2.9	Co=	1.0
Shear VLF=		65.3	<b>W6 ABs ok</b>

Upper- Main Floor			
H=	9.0	Mot=	75.8 k-ft
L=	20.0	C=	3.8 k
Vapp=	0.6	Mres=	72.9 k-ft
WW=	3.5	T=	0.1 k
TA=	8.0	AR=	1.2
Weight=	3.8	Co=	1.0
Shear VLF=		215.5	<b>W6 ABs ok</b>

8" CMU Wall at Basement

SW - G N/S Direction

Roof- Upper Floor			
H=	12.0	Mot=	44.4 k-ft
L=	20.0	C=	2.2 k
Vapp=	3.7	Mres=	41.6 k-ft
WW=	2.6	T=	0.2 k
TA=	6.0	AR=	1.2
Weight=	1.6	Co=	0.8
Shear VLF=		231.3	<b>W6 LSTA24</b>

SW - H E/W Direction

Roof- Upper Floor			
H=	11.0	Mot=	11.9 k-ft
L=	8.0	C=	1.5 k
Vapp=	1.1	Mres=	5.5 k-ft
WW=	1.0	T=	0.8 k
TA=	4.0	AR=	1.1
Weight=	0.4	Co=	1.0
Shear VLF=		135.0	<b>W6 HDU2</b>

Upper- Main Floor			
H=	9.0	Mot=	85.2 k-ft
L=	16.0	C=	5.3 k
Vapp=	0.8	Mres=	49.5 k-ft
WW=	4.1	T=	2.2 k
TA=	2.0	AR=	1.2
Weight=	2.0	Co=	1.0
Shear VLF=		283.1	<b>W6 HDU2</b>

Concrete Wall at Basement

Upper- Main Floor			
H=	9.0	Mot=	43.7 k-ft
L=	22.0	C=	2.0 k
Vapp=	2.5	Mres=	45.8 k-ft
WW=	3.1	T=	0.0 k
TA=	2.0	AR=	1.2
Weight=	1.1	Co=	1.0
Shear VLF=		160.5	<b>W6 ABs ok</b>

Concrete Wall at basement



SW - I E/W Direction

Roof- Upper Floor

H=	10.0	Mot=	25.1 k-ft
L=	12.0	C=	2.1 k
Vapp=	2.5	Mres=	11.5 k-ft
WW=	1.3	T=	1.4 k
TA=	4.0	AR=	1.1
Weight=	0.6	Co=	0.8
Shear VLF=		261.5	<b>W6 LSTA36</b>

Drag Strut Below

SW - K E/W Direction

Roof- Upper Floor

H=	12.0	Mot=	33.0 k-ft
L=	6.0	C=	5.5 k
Vapp=	2.8	Mres=	3.7 k-ft
WW=	0.8	T=	4.9 k
TA=	6.0	AR=	1.0
Weight=	0.5	Co=	1.0
Shear VLF=		458.3	<b>W4 MSTC66</b>

Upper- Main Floor

H=	9.0	Mot=	67.5 k-ft
L=	10.0	C=	6.7 k
Vapp=	1.1	Mres=	12.6 k-ft
WW=	1.7	T=	5.5 k
TA=	2.0	AR=	1.1
Weight=	0.8	Co=	1.0
Shear VLF=		383.0	<b>W6 HDU4</b>

Concrete Wall at Basement

SW - J E/W Direction

Roof- Upper Floor

H=	10.0	Mot=	17.3 k-ft
L=	14.0	C=	1.2 k
Vapp=	1.7	Mres=	15.7 k-ft
WW=	1.5	T=	0.1 k
TA=	4.0	AR=	1.2
Weight=	0.7	Co=	0.8
Shear VLF=		154.5	<b>W6 LSTA24</b>

Drag Strut Below

SW - L N/S Direction

Roof- Upper Floor

H=	12.0	Mot=	48.0 k-ft
L=	17.0	C=	2.8 k
Vapp=	4.0	Mres=	26.3 k-ft
WW=	2.2	T=	1.6 k
TA=	4.0	AR=	1.2
Weight=	0.9	Co=	0.8
Shear VLF=		294.1	<b>W6 LSTA36</b>

SW - M E/W Direction

Roof- Upper Floor

H=	11.0	Mot=	39.6 k-ft
L=	7.0	C=	5.7 k
Vapp=	3.6	Mres=	4.2 k-ft
WW=	0.8	T=	5.1 k
TA=	4.0	AR=	1.1
Weight=	0.4	Co=	1.0
Shear VLF=		514.3	<b>W4 MSTC66</b>

Upper- Main Floor

H=	9.0	Mot=	93.0 k-ft
L=	16.0	C=	5.8 k
Vapp=	1.0	Mres=	41.0 k-ft
WW=	3.8	T=	3.3 k
TA=	2.0	AR=	1.2
Weight=	1.4	Co=	1.0
Shear VLF=		312.5	<b>W6 HDU2</b>

Concrete Wall at Garage foundation

Upper- Main Floor

H=	6.0	Mot=	67.2 k-ft
L=	12.0	C=	5.6 k
Vapp=	1.0	Mres=	20.4 k-ft
WW=	1.6	T=	3.9 k
TA=	8.0	AR=	1.2
Weight=	1.8	Co=	1.0
Shear VLF=		383.3	<b>W6 HDU4</b>

SW - N N/S Direction

Roof- Upper Floor

H=	10.0	Mot=	42.8 k-ft
L=	7.0	C=	6.1 k
Vapp=	4.3	Mres=	3.9 k-ft
WW=	0.8	T=	5.6 k
TA=	4.0	AR=	1.1
Weight=	0.4	Co=	1.0
Shear VLF=		611.4	<b>W3 MSTC66</b>

SW - O E/W Direction

Main Floor- Basement

H=	9.0	Mot=	25.2 k-ft
L=	6.0	C=	4.2 k
Vapp=	2.8	Mres=	2.2 k-ft
WW=	0.6	T=	3.8 k
TA=	2.0	AR=	1.1
Weight=	0.2	Co=	1.0
Shear VLF=		466.7	<b>W4 HDU4</b>

Upper- Main Floor

H=	6.0	Mot=	76.3 k-ft
L=	14.0	C=	5.4 k
Vapp=	1.3	Mres=	25.8 k-ft
WW=	1.7	T=	3.6 k
TA=	8.0	AR=	1.2
Weight=	2.0	Co=	1.0
Shear VLF=		398.6	<b>W6 HDU4</b>

SW - P E/W Direction

Main Floor- Basement

H=	9.0	Mot=	18.9 k-ft
L=	8.0	C=	2.4 k
Vapp=	2.1	Mres=	3.9 k-ft
WW=	0.8	T=	1.9 k
TA=	2.0	AR=	1.1
Weight=	0.2	Co=	1.0
Shear VLF=		262.5	<b>W6 HDU2</b>

SW - Q E/W Direction

Main Floor - Crawlspace

H=	6.0	Mot=	6.0 k-ft
L=	22.0	C=	0.3 k
Vapp=	1.0	Mres=	22.0 k-ft
WW=	1.4	T=	0.0 k
TA=	2.0	AR=	1.2
Weight=	0.6	Co=	1.0
Shear VLF=		45.5	<b>W6 ABs ok</b>

Concrete Foundation Wall

SW - R E/W Direction

Main Floor- Basement

H=	9.0	Mot=	16.7 k-ft
L=	14.0	C=	1.2 k
Vapp=	1.9	Mres=	12.1 k-ft
WW=	1.4	T=	0.3 k
TA=	2.0	AR=	1.2
Weight=	0.4	Co=	1.0
Shear VLF=		132.9	<b>W6 ABs ok</b>

SW - S N/S Direction

Main Floor - Crawlspace

H=	8.0	Mot=	13.8 k-ft
L=	18.0	C=	0.8 k
Vapp=	1.7	Mres=	22.5 k-ft
WW=	1.6	T=	0.0 k
TA=	4.0	AR=	1.2
Weight=	0.9	Co=	1.0
Shear VLF=		95.6	<b>W6 ABs ok</b>

SW - T E/W Direction

Main Floor- Basement

H=	9.0	Mot=	14.1 k-ft
L=	17.0	C=	0.8 k
Vapp=	1.6	Mres=	17.8 k-ft
WW=	1.7	T=	0.0 k
TA=	2.0	AR=	1.2
Weight=	0.4	Co=	1.0
Shear VLF=		92.4	<b>W6 ABs ok</b>

SW - U E/W Direction

Roof- Upper Floor

H=	12.0	Mot=	23.0 k-ft
L=	4.0	C=	5.8 k
Vapp=	1.9	Mres=	1.5 k-ft
WW=	0.5	T=	6.2 k
TA=	4.0	AR=	0.9
Weight=	0.2	Co=	1.0
Shear VLF=		548.6	<b>W4 HDU5</b>

CMU Wall at FP BOX

Upper- Main Floor

H=	9.0	Mot=	49.3 k-ft
L=	6.0	C=	8.2 k
Vapp=	1.0	Mres=	6.1 k-ft
WW=	1.1	T=	7.2 k
TA=	8.0	AR=	1.1
Weight=	0.9	Co=	1.0
Shear VLF=		486.7	<b>W4 HDU5</b>

CMU Wall at FP BOX

SW - V E/W Direction

Roof- Upper Floor

H=	11.0	Mot=	49.7 k-ft
L=	5.0	C=	9.9 k
Vapp=	4.5	Mres=	2.1 k-ft
WW=	0.6	T=	9.8 k
TA=	4.0	AR=	1.0
Weight=	0.3	Co=	1.0
Shear VLF=		927.2	<b>W2 HDU8</b>

Upper- Main Floor

H=	9.0	Mot=	102.1 k-ft
L=	6.0	C=	17.0 k
Vapp=	1.3	Mres=	6.5 k-ft
WW=	1.2	T=	15.9 k
TA=	8.0	AR=	1.1
Weight=	1.0	Co=	1.0
Shear VLF=		970.0	<b>W2 NG</b>

SW - X N/S Direction

Roof- Main Floor

H=	8.0	Mot=	8.8 k-ft
L=	4.5	C=	2.0 k
Vapp=	1.1	Mres=	1.2 k-ft
WW=	0.4	T=	1.7 k
TA=	2.5	AR=	1.0
Weight=	0.1	Co=	1.0
Shear VLF=		244.4	<b>W6 HDU2</b>

SW - Y E/W Direction

Roof- Main Floor

H=	9.0	Mot=	19.8 k-ft
L=	6.0	C=	3.3 k
Vapp=	2.2	Mres=	2.7 k-ft
WW=	0.6	T=	2.9 k
TA=	4.0	AR=	1.1
Weight=	0.3	Co=	1.0
Shear VLF=		366.7	<b>W6 HDU2</b>

SW - Z N/S Direction

Roof- Main Floor

H=	9.0	Mot=	11.7 k-ft
L=	6.0	C=	2.0 k
Vapp=	1.3	Mres=	2.3 k-ft
WW=	0.6	T=	1.6 k
TA=	2.5	AR=	1.1
Weight=	0.2	Co=	1.0
Shear VLF=		216.7	<b>W6 HDU2</b>

SW - AA E/W Direction

Terrace- Basement

H=	9.0	Mot=	5.4 k-ft
L=	7.0	C=	0.8 k
Vapp=	0.6	Mres=	3.7 k-ft
WW=	0.7	T=	0.4 k
TA=	4.0	AR=	1.1
Weight=	0.4	Co=	0.7
Shear VLF=		122.4	<b>W6 ABs ok</b>

Diaphragm Checks for Collector elements at High Roofs

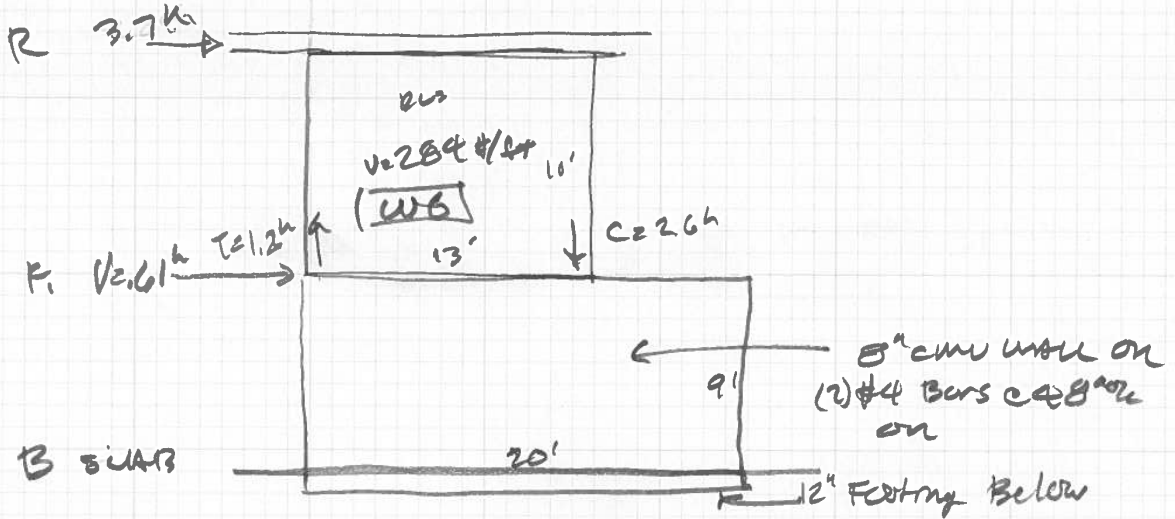
Shear Wall	Force Applied	Multiplier per 12.3.3.4	diaphragm capacity	Collector Length	Check	Load Applied to SW
A	1.38	1.25	0.61	43	OK	1.794
B	1.94	1.25	0.61	8	OK	2.522
C center	5.11	1.25	0.61	10		6.643
C west	1.4	1.25	0.61	10	OK	1.82
D	3.67	1.25	0.61	24	OK	4.771
E	1.56	1.25	0.61	11	OK	2.028
F	2.84	1.25	0.61	13	OK	3.692
G	2.84	1.25	0.61	39	OK	3.692
H	1.08	1.25	0.61	8	OK	1.404
I	1.93	1.25	0.61	12	OK	2.509
J	1.33	1.25	0.61	14	OK	1.729
K	2.11	1.25	0.61	12	OK	2.743
L	3.98	1.25	0.61	17	OK	5.174
M	3.57	1.25	0.61	12	OK	4.641
N	4.28	1.25	0.61	7.5		8.8
U	1.48	1.25	0.61	3		3.0
V	3.48	1.25	0.61	4		7.1
W	5.86	1.25	0.61	8		12.0
X	0.85	1.25	0.61	4	OK	1.105
Y	1.69	1.25	0.61	6	OK	2.197
Z	1	1.25	0.61	6	OK	1.3

SHEAR WALL F - WOOD TO CMU LATERAL SAMPLE

$V_R = 2.84k$  ( $R=6.5$ , WOOD SW) from Diaphragm Dist

$= 3.69k$  w/  $R=5$

$V_F = 0.47k$  (w/  $R=6.5$ ) =  $0.611k$  w/  $R=5$



I.L. GROSS  
STRUCTURAL  
ENGINEERS

SHEAR WALL - F w/ R=5.0 For CMU

SHEET TITLE

Lake Home

PROJECT

[Signature]

CLIENT

SCALE

MARK

DESIGNED BY

CHECKED

6/2021

DATE



SHEET

Mark Speidel, PE, SE  
 I.L. Gross Structural Engineers LLC  
 23914 56th Ave W Suite 200  
 Mountlake Terrace, WA  
 www.ilgross.com

Project Title: **Lorenzini Waterfront Home**  
 Engineer: **Mark Speidel**  
 Project ID:  
 Project Descr: **SFR Remodeling**

## Masonry Shear Wall

File: Lorenzini Residence.ec6

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I.L. GROSS STRUCTURAL ENGINEERS

Lic. #: KW-06002858

**DESCRIPTION:** Masonry SW-F with R=5.0

### Code References

Calculations per TMS 402-16, IBC 2018, CBC 2019, ASCE 7-16  
 Load Combinations Used : ASCE 7-16

### General Information

Wall Material	MASONRY	f <sub>m</sub>	1.50 ksi	Block Class	
Total Wall Height	9.0 ft	F <sub>y</sub> - Rebar	60.0 ksi	Concrete Density	150.0 pcf
Base Wall Length	20.0 ft	F <sub>y</sub> - HJR	70.0 ksi	Min. Bending As %	0.00180
R: Resp. Mod Factor	5.0	Em	3,120.0 ksi		
Ie: Seismic Import. Factor	1.0	Phi - Shear	0.80	Phi : Axial & Flexure	0.90

### Wall Data

#### Bottom

Analysis Height	0.00 ft
Wall Offset	( datum ) ft
Wall Length	20.0 ft
Effective Length 'd'	232.0 in
Nominal Block Thickness	8 in
Solid Grout?	Partial Groute

#### Reinforcing in Field of Wall

Vertical Bar Size #	4
Vertical Bar Spacing	32 in
Horiz. joint reinf. area (HJR)	0.55 in
HJR Spacing	48 in
Bond beam reinf. area	0.4 in
Spacing of bond beams	48 in

#### In each chord cell:

Vertical rebar size #	4
# Chord Cells @ Each End	2

**Masonry Shear Wall**

File: Lorenzini Residence.ec6

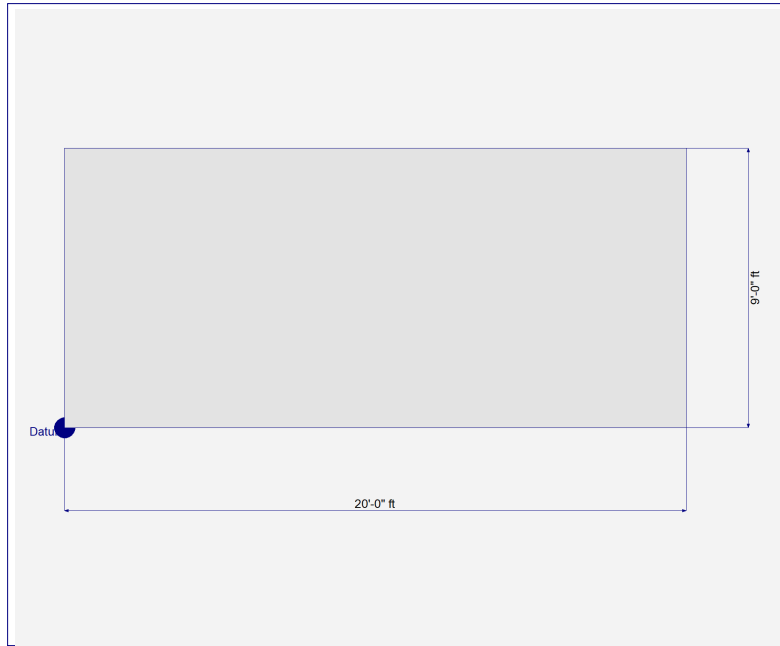
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DESCRIPTION: Masonry SW-F with R=5.0

**Wall Sketch**



**Applied Concentrated Vertical Loads**

Load Location (ft)		Dead Load	Load Magnitude (kips)			Snow Load	Earth Load
X Location	Y Location		Roof Live Load	Live Load			
	9.0	1.560		3.60			

**Applied Distributed Vertical Loads**

Load Location (ft)		Height of Application	Load Magnitude (kips)			Snow Load	Earth Load
Start Location	End Location		Dead Load	Roof Live Load	Live Load		
	20.0	9.0	0.1360		0.320		
	13.0	9.0	0.2480			0.2520	

**Applied Concentrated Lateral Loads**

Load "Y" Location (ft)	Dead Load	Load Magnitude (kips)			Wind Load	Seismic Load	Earth Load
		Roof Live Load	Floor Live Load				
9.0						3.690	
9.0						0.620	

## Masonry Shear Wall

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Lic. #: KW-06002858

**DESCRIPTION:** Masonry SW-F with R=5.0

### SHEAR ANALYSIS

	<u>Bottom Level</u>
Special Boundary	
Elements Req'd?	Not Req'd
Vu : Story Shear	4.310 k
for Load Combination	+1.20D+L+0.20S+E
Controlling Mu/(Vud)	1.00
Vn Masonry	119.988 k
Vn Steel	27.0 k
Vn Masonry + Vn Steel	146.988 k
Vn Max	146.678 k
Phi Vn	117.342 k
Ratio: Vu/PhiVn (controlling)	
Vertical As >= Av/3	OK
Vertical Bar Spacing <= 96"	OK

### AXIAL ANALYSIS

	<u>Bottom Level</u>
H / d Ratio	0.47
Pu	39.920 k
for Load Combination	+1.20D+1.60L+0.50S
Phi Pn	117.342 k
Ratio: Pu/PhiPn (controlling)	<b>0.02817</b>

### BENDING ANALYSIS

	<u>Bottom Level</u>
"a" : Flexural compression	2.62 in
Length of defined chord zone is >= the "a" dimension of the masonry (the compression zone)	OK
"d" : Eff depth to tension reinf	232.0
As-flex < As-max ?	0.400 <= 15.676
Mu	95.594 k
for Load Combination	+1.20D+1.60L+0.50S
Phi Mn	415.239 k
Ratio: Mu/PhiMn (controlling)	<b>0.2302</b>

### Force Summary

Load Combination	Wall Level	Values for Wall section			Resultant Ecc (ft)	Overturning Ratio	Uplift (k)	
		Vu (k)	Mu (k)	Pu (k)			Left	Right
+1.40D	Wall Level : 1		37.638	25.995	1.448			
+1.20D+1.60L	Wall Level : 1		89.861	38.282	2.347			
+1.20D+1.60L+0.50S	Wall Level : 1		95.594	39.920	2.395			
+1.20D+L	Wall Level : 1		68.261	32.282	2.115			



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Project Title: **Lorenzini Waterfront Home**  
 Engineer: **Mark Speidel**  
 Project ID:  
 Project Descr: **SFR Remodeling**

## Masonry Shear Wall

File: Lorenzini Residence.ec6

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Lic. #: KW-06002858

**DESCRIPTION:** Masonry SW-F with R=5.0

### Force Summary

Load Combination	Wall Level	Values for Wall section			Resultant Ecc (ft)	Overturning Ratio	Uplift (k)	
		Vu (k)	Mu (k)	Pu (k)			Left	Right
+1.20D	Wall Level : 1		32.261	22.282	1.448			
+1.20D+L+1.60S	Wall Level : 1		86.606	37.523	2.308			
+1.20D+1.60S	Wall Level : 1		50.606	27.523	1.839			
+1.20D+L+0.50S	Wall Level : 1		73.994	33.920	2.181			
+0.90D	Wall Level : 1		24.196	16.711	1.448			
+1.20D+L+0.20S+E	Wall Level : 1	4.310	31.764	32.937	0.964	9.739		
+0.90D+E	Wall Level : 1	4.310	14.594	16.711	0.873	5.217	1.028	1.028

### Footing Information

#### Footing Dimensions

Dist. Left	2.0 ft	fc	2.50 ksi	Rebar Cover	3.0 in
Wall Length	20.0 ft	Fy	60.0 ksi	Footing Thickness	12.0 in
Dist. Right	2.0 ft			Width	1.50 ft
Total Ftg Length	24.0 ft				

#### Max Factored Soil Pressures

@ Left Side of Footing	3,553.56 psf
.... governing load comb	+1.20D+1.60L+0.50S
@ Right Side of Footing	1,396.82 psf
.... governing load comb	+1.20D+L+0.20S+E

#### Max Unfactored Soil Pressures

@ Left Side of Footing	2,507.34 psf
.... governing load comb	+D+L
@ Right Side of Footing	1,064.82 psf
.... governing load comb	+D+0.750L+0.750S+0.5250E

#### Footing One-Way Shear Check...

vu @ Left End of Footing	47.552 psi
vu @ Right End of Footing	19.416 psi
vn * phi : Allowable	85.0 psi

#### Overturning Stability...

	<b>@ Left End of Ftg</b>	<b>@ Right End of Ftg</b>
Overturning Moment	33.365 k-ft	33.365 k-ft
Resisting Moment	148.663 k-ft	180.924 k-ft
Stability Ratio	4.456 : 1	5.423 : 1
.... governing load comb	+0.60D+0.70E	+0.60D+0.70E

#### Footing Bending Design...

	<b>@ Left End</b>	<b>@ Right End</b>
Mu	10.464 k-ft	4.284 k-ft
Ru	95.697 psi	39.173 psi
As % Req'd	0.00180 in^2	0.00180 in^2
As Req'd in Footing Width	0.3888 in^2	0.3888 in^2

**Multiple Simple Beam**

Lic. #: KW-06002858

**Description :** Rev2 Permit Corr Calcs

**Wood Beam Design :** Garage Ceiling Joists

Calculations per NDS 2018, IBC 2018, CBC 2019, ASCE 7-16

BEAM Size : **2x6, Sawn, Braced @ 1/3 Points**

Using Allowable Stress Design with ASCE 7-16 Load Combinations, Major Axis Bending

Wood Species : DouglasFir-Larch

Wood Grade : No.2

Fb - Tension	900.0 psi	Fc - Prll	1,350.0 psi	Fv	180.0 psi	Ebend- xx	1,600.0 ksi	Density	31.210 pcf
Fb - Compr	900.0 psi	Fc - Perp	625.0 psi	Ft	575.0 psi	Eminbend - xx	580.0 ksi		

Applied Loads

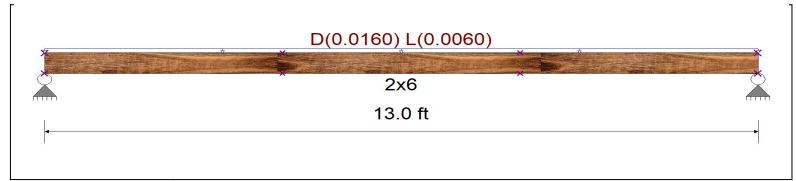
Unif Load: D = 0.0080, L = 0.0030 k/ft, Trib= 2.0 ft

Design Summary

Max fb/Fb Ratio = **0.652** : 1  
 fb : Actual : 737.45 psi at 6.500 ft in Span # 1  
 Fb : Allowable : 1,131.87 psi  
 Load Comb : +D+L

Max fv/FvRatio = **0.135** : 1  
 fv : Actual : 24.27 psi at 12.567 ft in Span # 1  
 Fv : Allowable : 180.00 psi  
 Load Comb : +D+L

Max Reactions (k)	D	L	Lr	S	W	E	H
Left Support	0.10	0.04					
Right Support	0.10	0.04					



Max Deflections

Transient Downward	0.116 in	Total Downward	0.427 in
Ratio	1339	Ratio	365
LC: L Only		LC: +D+L	
Transient Upward	0.000 in	Total Upward	0.000 in
Ratio	9999	Ratio	9999
LC:		LC:	

**Wood Beam Design :** Garage Ceiling Beam

Calculations per NDS 2018, IBC 2018, CBC 2019, ASCE 7-16

BEAM Size : **2-2x8, Sawn, Braced @ 1/3 Points**

Using Allowable Stress Design with ASCE 7-16 Load Combinations, Major Axis Bending

Wood Species : DouglasFir-Larch

Wood Grade : No.2

Fb - Tension	900.0 psi	Fc - Prll	1,350.0 psi	Fv	180.0 psi	Ebend- xx	1,600.0 ksi	Density	31.210 pcf
Fb - Compr	900.0 psi	Fc - Perp	625.0 psi	Ft	575.0 psi	Eminbend - xx	580.0 ksi		

Applied Loads

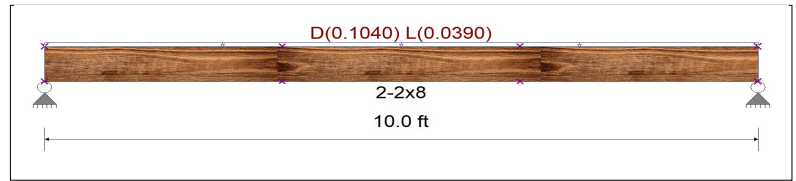
Unif Load: D = 0.0080, L = 0.0030 k/ft, Trib= 13.0 ft

Design Summary

Max fb/Fb Ratio = **0.760** : 1  
 fb : Actual : 816.17 psi at 5.000 ft in Span # 1  
 Fb : Allowable : 1,073.87 psi  
 Load Comb : +D+L

Max fv/FvRatio = **0.241** : 1  
 fv : Actual : 43.39 psi at 9.400 ft in Span # 1  
 Fv : Allowable : 180.00 psi  
 Load Comb : +D+L

Max Reactions (k)	D	L	Lr	S	W	E	H
Left Support	0.52	0.20					
Right Support	0.52	0.20					

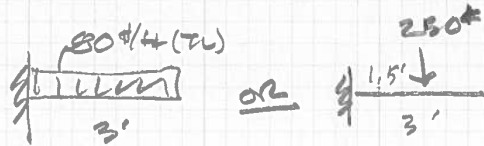


Max Deflections

Transient Downward	0.058 in	Total Downward	0.212 in
Ratio	2073	Ratio	565
LC: L Only		LC: +D+L	
Transient Upward	0.000 in	Total Upward	0.000 in
Ratio	9999	Ratio	9999
LC:		LC:	

# FLOATING STAIR DESIGN

TREAD WT = 20# PL  
 LL = 60# PL  
 OR (1) 250# PL



$$M_U = 1.2D + 1.6L = 120 \text{ plf} \times 3' \times \frac{3'}{2} = 540 \text{ ft}^2 = 6.48 \text{ k}^2$$

$$M_U = 1.2D + 1.6(PL) = 24 \times 3 \times 1.5 + 400 \times 1.5 = 708 \text{ ft}^2 = 8.49 \text{ k}^2 \leftarrow \text{governs}$$

$\phi F_y = 45 \text{ ksi}$  (for GR A992 W sections)

$S_x \text{ min} = 0.19 \text{ in}^3$

$$\Delta_{TL} = \frac{1}{240} = 0.15'' = \frac{20 \times 3' \times 36^3}{8EI} + \frac{250 \text{ lb} \times 18''^2}{6EI} \quad (3 \times 36 - 18)$$

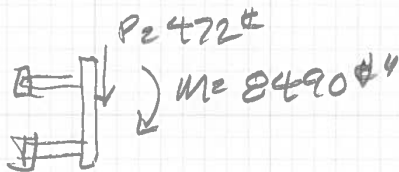
$$= \frac{349920}{EI} + \frac{1215000}{EI} = \frac{0.054}{I} \leq 0.15$$

$$I_{\text{min}} = 0.36 \text{ in}^4$$

WT 4x14  $S_x = 1.28 > 0.19$   
 $I = 4.23 > 0.36$

✓ WT 4x14 IS OK

## EMBED PL



1/2" x 2" x 7" EMBED PL w/ (4) 3/4" x 6" STUBS OK  
 (see PROF'S CUTAWAY)



I.L. GROSS  
 STRUCTURAL  
 ENGINEERS

Floating Stair Calculation

SHEET TITLE

Loenenmi

PROJECT

Bob Swann

CLIENT

SCALE

MARCH

DESIGNED BY

CHECKED

4/20/21

DATE



SHEET

[www.hilti.us](http://www.hilti.us)

Company: I.L. Gross Structural Engineers  
 Specifier: Mark Speidel  
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 Phone | Fax: 425-640-7333 |  
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Page: 1  
 Project: Lorenzini Residence  
 Sub-Project | Pos. No.: Floating Stair Embed  
 Date: 6/7/2021

**Specifier's comments:** Embed PL into CMU wall for floating stair tread

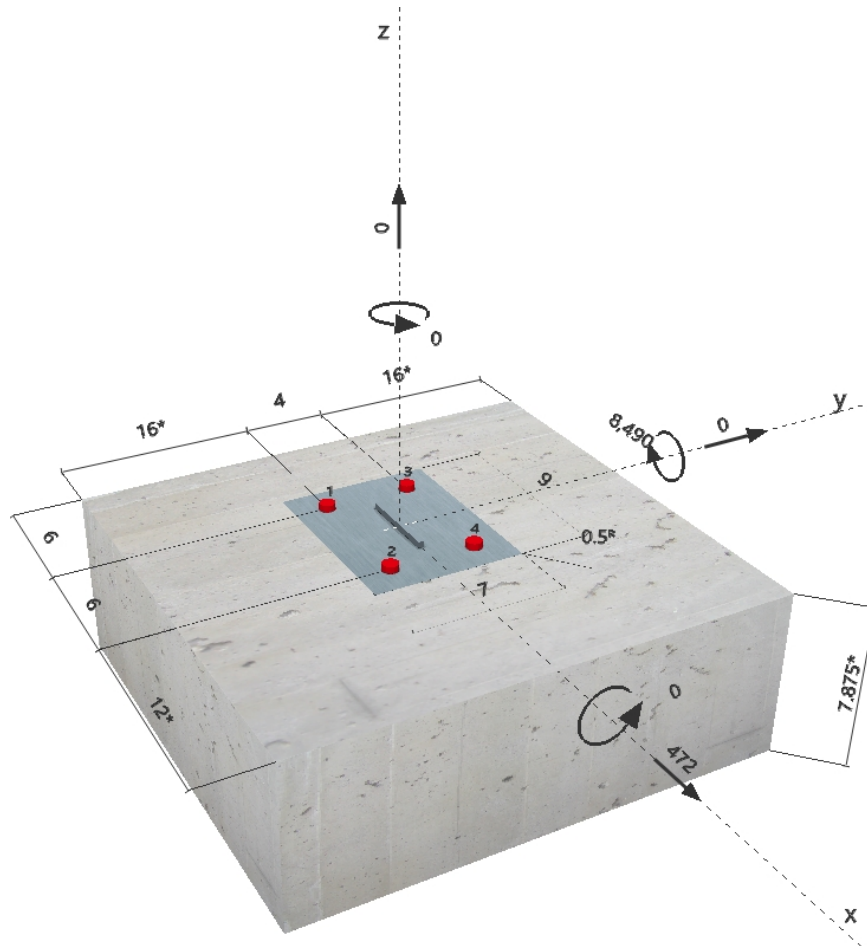
## 1 Input data

<b>Anchor type and diameter:</b>	<b>AWS D1.1 GR. B 3/4</b>
Effective embedment depth:	$e_{ef} = 5.000$ in.
Material:	
Proof:	Design method ACI 318-14 / CIP
Stand-off installation:	$e_b = 0.000$ in. (no stand-off); $t = 0.500$ in.
Anchor plate:	$l_x \times l_y \times t = 9.000$ in. $\times$ $7.000$ in. $\times$ $0.500$ in.; (Recommended plate thickness: not calculated)
Profile:	Rectangular plates and bars (AISC); (L x W x T) = $4.000$ in. $\times$ $0.250$ in. $\times$ $0.000$ in.
Base material:	cracked concrete, 2000, $f'_c = 2,000$ psi; $h = 7.875$ in.
Reinforcement:	tension: condition B, shear: condition A; edge reinforcement: $\geq$ No. 4 bar



<sup>R</sup> - The anchor calculation is based on a rigid baseplate assumption.

### Geometry [in.] & Loading [lb, in.lb]



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## 2 Proof I Utilization (Governing Cases)

Loading	Proof	Design values [lb]		Utilization	
		Load	Capacity	$\beta_N / \beta_V$ [%]	Status
Tension	Concrete Breakout Strength	1,294	9,001	15 / -	OK
Shear	Concrete edge failure in direction x+	472	9,960	- / 5	OK

Loading	$\beta_N$	$\beta_V$	$\zeta$	Utilization $\beta_{N,V}$ [%]	Status
Combined tension and shear loads	0.144	0.047	5/3	5	OK

## 3 Warnings

- Please consider all details and hints/warnings given in the detailed report!

## Fastening meets the design criteria!

## 4 Remarks; Your Cooperation Duties

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